

Technologies for the Design and Operation of Phosphate Fertilizer & Sulfuric Acid Plants

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INTRODUCTION

A global economic crisis has caused a sell-off in commodities in recent months. Fertilizer inventory levels are high because of lower demand. There is a need in the market to produce high value products at lower costs. Technology is fundamental to the profitable design and operation of environmentally friendly phosphate and sulfuric acid plants and processes. In this study we will examine how modeling technology can help in debottlenecking existing plants, achieving high product purity, increasing energy recovery, and automate process analysis to optimize plant operations.

Models for sulfuric and phosphoric acid plants will be examined with reference to physical property estimation methods, representation of unit operations in the plant, online analytical measurements and process optimization. Sulfuric acid plants are net producers of steam; it will be determined how effective decisions on steam boilers can be made using sulfuric acid plant models.

aspenONE ENGINEERING FOR CHEMICALS

aspenONE Engineering enables engineers to model the sulfuric acid and phosphoric acid processes in one integrated environment. Process Engineering has been successfully utilized by plant owners/operators, engineering and construction companies, and technology providers to improve yields, increase plant efficiency and quality, and reduce capital and operating costs.

Operation of a sulfuric acid facility can be challenging because of the high cost of maintenance of sulfuric acid plants, stringent requirements on SO₂ emissions, importance of energy efficiency, and accurate equipment sizing and rating. aspenONE Engineering has been successfully used by many companies to design every sub-process of the sulfuric and phosphoric acid plant in one integrated environment.

Aspen Plus is an integral part of aspenONE Engineering and contains the world's largest database of pure components and phase equilibrium data for conventional chemicals, electrolytes, solids, and polymers. The physical property database is regularly updated with data from the U. S. National Institute of Standards and Technology (NIST). Having accurate physical properties data is critical to the precision of the simulation results and directly affects the cost of process equipment. The electrolytes feature in Aspen Plus improves the accuracy of the vapor-liquid equilibrium calculations in the adsorption units of sulfuric and phosphoric acid processes.

Figure 1 illustrates the overall engineering workflow and life cycle process of designing a sulfuric acid plant. Based on the process concept and business objective, one can establish the performance of the concept and then improve the concept using

conceptual design methodologies in Aspen Plus. The base case and the improved case economic feasibility can be compared using standard cost analysis environment such as Aspen Process Economics Analyzer. It is also important to establish a detailed performance model for critical equipment. This helps identify a practical design option during the conceptual phase. The basis for these detailed equipment models needs to be consistent between the base case and the improved case.

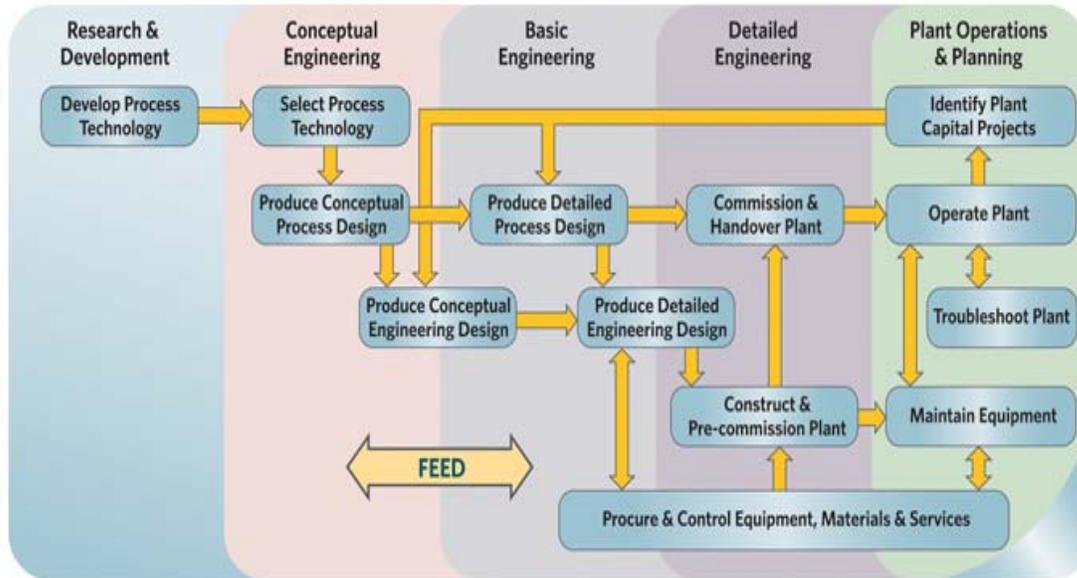


Figure 1: Engineering Workflow

After developing an improved process concept, Aspen Plus Dynamics can then test the process for safety, operability, and controllability issues; this defines the key control loops and the instrumentation for the process. Once the process control strategy and key instrumentation is defined, the definition of the process intent for the design is complete.

Aspen Basic Engineering can then be used to develop the FEED package, incorporating the PFD or process P&ID for the improved concept, equipment designs, data sheets, summary sheets and basic control loops and instrumentation. The process design information can then be further transferred into detailed P&ID and instrumentation environments.

The performance models developed for the process can be re-used for operational monitoring and improvement of the plant using Aspen Simulation Workbook. The performance model can also be deployed to non-expert users who may not have background in simulation to perform “what if analysis” studies over the web using Aspen Online Deployment ⁽¹⁾.

IMPORTANCE OF PHYSICAL PROPERTIES

Sulfuric acid has consistently ranked #1 in world chemical production. Considerable work has been done in the steady state simulation area of sulfuric acid processes. Sulfuric acid models have been used to design, de-bottleneck, and troubleshoot plants, converter profile optimization (with the Equation Oriented (EO) capability), evaluate catalyst purchases and rate present catalyst condition, energy recovery analysis, and to emulate gas-to-gas hex leaks. Some of the key variables in sulfuric acid production are: gas strength, production rate, stack SO₂, converter catalyst loading and temperature profile, acid strength, steam production, gas pressure drop, and gas dew-point.

Physical properties are the most important part of any simulation, it is critical to have accurate and updated physical properties to perform engineering calculations which eventually dictate the sizing and rating of plant equipment which affects the capital costs, operating costs, and safety of the plant.

Aspen Properties is part of aspenONE Engineering and provides state-of-the-art physical property methods, models, algorithms, and data that enables chemists and engineers to easily perform engineering calculations based on rigorous and proven thermophysical property models and data. It enables users to capture and deploy consistent physical property data and knowledge across the enterprise. Aspen Properties contains the world's largest database of pure components and binary parameter databanks.

For simulation aqueous acids such as sulfuric acid and phosphoric acid processes it is recommended to turn the electrolytes feature on in Aspen Plus. In Aspen Plus, an electrolyte system is defined as one in which some of the molecular species dissociates partially or completely into ions in a liquid solvent, and/or some of the molecular species precipitate as salts. These dissociation and precipitation reactions occur fast enough that the reactions can be considered to be at chemical equilibrium. The liquid phase equilibrium reactions that describe this behavior are referred to as the solution chemistry. In Aspen Plus, solution chemistry is often referred to simply as Chemistry⁽²⁾.

Solution chemistry has a major impact on the simulation of electrolyte systems. For non-electrolyte systems, chemical reactions generally occur only in reactors. In Aspen Plus, all unit operation models can handle electrolyte reactions⁽²⁾.

Solution chemistry also impacts physical property calculations and phase equilibrium calculations. The presence of ions in the liquid phase causes highly non-ideal thermodynamic behavior. Aspen Plus provides specialized thermodynamic models and built-in data to represent the non-ideal behavior of liquid phase components in order to get accurate results⁽²⁾.

EQUATION ORIENTED MODELING

Sequential Modeling (SM) is the traditional approach of modeling in Aspen Plus; SM solves each block in the flowsheet in sequence. SM is a viable option generally for flowsheets without too many recycle loops. However for larger flowsheets with multiple recycle loops SM can be very time consuming.

Unlike SM Equation Oriented (EO) modeling does not solve each block in sequence. EO gathers all the model equations together and solves them together. EO is typically ideal for highly heat-integrated processes, process with multiple recycle loops, processes with numerous design specifications, process optimization, and for process model tuning through data reconciliation and parameter estimation. EO solves much larger problems than SM and uses the same computational effort⁽³⁾.

RATE BASED DISTILLATION

Aspen Rate-Based Distillation (formerly Aspen RateSep) is part of the aspenONE Engineering solution, and extends the functionality of Aspen Plus RadFrac distillation model with second-generation rate-based technology which accurately predicts simulation over a wide range of operating conditions. Aspen Rate Based Distillation uses state-of-the-art mass- and heat transfer correlations to predict column performance, without the need of efficiency factors. This added degree of rigor is especially critical for modeling gas scrubbers, sour water strippers, azeotropic systems, reactive distillations, nitric acid absorption columns, narrow-boiling separations, and other highly non-ideal separation processes.

The rate-based modeling approach is superior to the traditional equilibrium-stage modeling approach that has been employed extensively in the process industries. The rate-based models assume that separation is caused by mass transfer between the contacting phases, and use the Maxwell-Stefan theory to calculate mass transfer rates. Conversely, the equilibrium-stage models assume that the contacting phases are in equilibrium with each other, which is an inherent approximation because the contacting phases are never in equilibrium in a real column.

The rate-based modeling approach has many advantages over the equilibrium-stage modeling approach. The rate-based models represent a higher fidelity, more realistic modeling approach and the simulation results are more accurate than those attainable from the equilibrium-stage models. The rate-based modeling approach can reduce the risk of inadequate designs or off-spec operation because the rate-based models explicitly account for the actual column configuration which affects column performance.

Designed to model reactive multistage separation problems rigorously and accurately, Aspen Rate-Based Distillation balances gas and liquid phase separately and considers mass and heat transfer resistances according to the film theory by explicit calculation of interfacial fluxes and film discretization. The film model equations are combined with relevant diffusion and reaction kinetics and include the specific features

of electrolyte solution chemistry, electrolyte thermodynamics, and electroneutrality where appropriate. The hydrodynamics of the column is accounted for via correlations for interfacial area, hold-up, pressure drop, and mass transfer coefficients. SO₂ stripping is a rate-limited process, and can be accurately modeled using Aspen Rate-Based Distillation⁽¹⁾⁽⁴⁾.

STEADY-STATE SULFURIC ACID MODEL

This model simulates the production process of sulfuric acid from sulfur in a typical double absorption plant. The model includes the following features:

- A set of electrolyte components for this process
- Typical process areas including: sulfur burning, sulfur dioxide conversion, absorption of sulfur trioxide and the main streams connecting these units.
- Definition of methods for calculating and reporting electrolyte systems
- Supports rigorous design, rating, or simulation by interfacing with the A program.

Components: The table below lists the components modeled in the simulation.

Components	Component ID Type	Component name	Formula
H ₂ O	CONV	Water	H ₂ O
H ₂ SO ₄	CONV	Sulfuric acid	H ₂ SO ₄
SO ₂	CONV	Sulfur dioxide	O ₂ S
SO ₃	CONV	Sulfur trioxide	O ₃ S
S	CONV	Sulfur	S
N ₂	CONV	Nitrogen	N ₂
O ₂	CONV	Oxygen	O ₂
C ₁₀ H ₂₂	CONV	n-Decane	C ₁₀ H ₂₂ -1
H ₃ O ⁺	CONV	Hydronium ion	H ₃ O ⁺
HSO ₄ ⁻	CONV	Bisulfate ion	HSO ₄ ⁻
SO ₄ ⁻⁻	CONV	Sulfate ion	SO ₄ ⁻²
CO ₂	CONV	Carbon-Dioxide	CO ₂

SO₂, O₂, N₂ and CO₂ are selected Henry's components. The Electrolytes Expert System can be used to generate electrolyte species and reactions. In this model, acidic species are treated as hydronium ion H₃O⁺ and choose components H₂O and H₂SO₄ for the electrolytes system. In addition, we use the apparent component approach.

Process Description: Figure 2 shows the process flowsheet which includes: air drying, sulfur burning, sulfur dioxide conversion, double absorption of sulfur trioxide, gas-to-gas heat exchangers, strong acid system and energy recovery system (steam system).

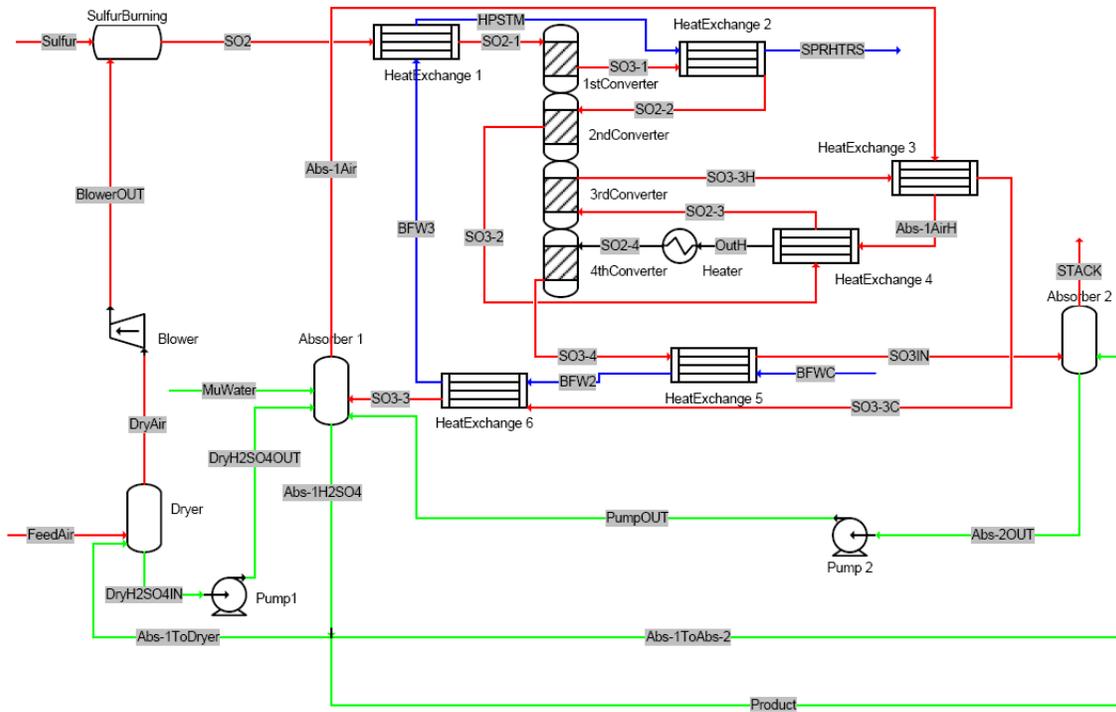


Figure 2: Sulfuric Acid Process Flowsheet

Sulfur is mixed with the dry air after the removal of water from the feed air in the drying column. An oxidation reaction takes place in the sulfur burner. Then the sulfur dioxide gas and the unreacted air are cooled from 2010F to 750F prior to entering the first pass of the converter where sulfur dioxide is converted to sulfur trioxide.

Sulfur dioxide and air undergo the catalytic oxidation reaction in the converter. Since the heat released from the sulfur dioxide oxidation will increase the temperature of the catalysts, the equilibrium conversion rate will decrease. So the sulfur dioxide conversion process is divided into 4 stages and the temperature of the catalysts in each stage can be kept suitable by stepwise cooling among the stages. Thus the reaction can get higher conversion and reaction rate.

In, the double absorption process, the gas (SO₂, air and SO₃) from the third converter pass enters the inter-pass tower. After the generated sulfur trioxide is absorbed, the residual gas (SO₂, air) is heated again and enters into the fourth pass of the converter. The inter-pass absorber removes the SO₃ so the conversion in the fourth pass of the converter is increased. The gas out from the fourth pass of the converter enters the final absorption column. Stack SO₂ concentration is lowered below 500ppm so the exhaust gas can be discharged to atmosphere.

The sulfuric acid (98.5%) from the inter-pass absorption column splits into three streams including the product stream, stream Abs-1ToDryer and stream Abs-1ToAbs-2. Stream Abs-1ToDryer will go to the dry column as de-hydrant. Stream Abs-1ToAbs-2

will go to the final absorption column as the absorbent. The sulfuric acid solution (98.9%) from the final absorption column and the sulfuric acid solution (97.7%) from the dry column will both enter the inter-pass absorption column as absorbent.

Process summary

Area	Purpose
Dryer	Dry feed air
Sulfur Burning	Preparation of sulfur dioxide
Sulfur Dioxide Conversion	Preparation of sulfur trioxide
Absorption of Sulfur Trioxide	Preparation of sulfuric acid
Steam System	Heat removal and steam generation

Physical Properties: The global property option used in this model is ELECNRTL. This option set is used for the simulations with non-ideal electrolyte solutions. ELECNRTL calculates liquid phase properties from the Electrolyte-NRTL activity coefficient model. Also, Henry's Law is used to calculate gas (SO₂, O₂, N₂ and CO₂) solubility in sulfuric acid. The Ideal property option is used for vapor phase at high temperature in the converter and heater unit operation. The STEAMNBS property option is used for the steam system (economizers, boiler, and superheater) unit operations.

Chemical Reactions: The chemical reactions in this process include gas reactions, absorption reactions and acid chemistry. The reactors are modeled with the built-in models RGibbs for the sulfur burner, and RCSTR for the converter passes. And the sulfur trioxide absorption reaction takes place in RadFrac column. The table below lists the reaction units and corresponding Aspen Plus models:

Reaction Unit	Reaction Type	Aspen Plus Model
Sulfur Burn	Equilibrium	Rgibbs
Converters	Kinetic	RCSTR
Absorption reaction	Equilibrium	RadFrac

Reactions in each reactor and their specifications in Aspen Plus model are listed as follows:

Sulfur Burn

Component	Valid Phases
N ₂	Vap
O ₂	Vap
SO ₂	Vap
CO ₂	Mixed
H ₂ O	Mixed

Sulfur Burn is modeled using the Gibbs free energy minimum method in the RGibbs model. This determines the equilibrium composition of the products resulting from the many reactions that can occur.

Converters

Rxn No.	Specification type	Stoichiometry
1	Kinetic	$\text{SO}_2 + 0.5\text{O}_2 \rightarrow \text{SO}_3$

The four converter passes in this process are modeled using four RCSTR reactors with user reaction kinetics. FORTRAN subroutine USRKIN represents the kinetics in all converter passes. USRKIN is included compiled and linked in file Rate1.dll. File sulfuric.opt holds the pointer to the .dll file. It is recommended you place all three files (.bkp, .dll, and .opt) in the same directory.

Converter	Reaction ID	Subroutine Name	Values for parameters
1 st	Rate1	USRKIN	Integer Real 1 27000 2 1.8
2 nd	Rate2	USRKIN	Integer Real 1 31000 2 1.8
3 rd	Rate3	USRKIN	Integer Real 1 30000 2 1.8
4 th	Rate4	USRKIN	Integer Real 1 42000 2 1.8

The first Real parameter of USRKIN is the volume of catalyst in liters. The second Real parameter is the activity of the catalyst. You may adjust these parameters to calibrate the model to reflect the performance of your plant.

Absorption Reaction

Reaction	Type	Stoichiometry
1	Equilibrium	$\text{SO}_3 + \text{H}_2\text{O} \rightleftharpoons \text{H}_2\text{SO}_4$

Absorption reaction is modeled using Radfrac.

Acid Chemistry

Reaction	Type	Stoichiometry
1	Equilibrium	$\text{H}_2\text{SO}_4 + \text{H}_2\text{O} \rightleftharpoons \text{H}_3\text{O}^+ + \text{HSO}_4^-$
2	Equilibrium	$\text{HSO}_4^- + \text{H}_2\text{O} \rightleftharpoons \text{H}_3\text{O}^+ + \text{SO}_4^{--}$

Ionic equilibrium reactions in the liquid phase are modeled using Chemistry and the apparent components approach.

Simulation Approach:

Unit Operations – The major unit operations are represented by Aspen Plus models as shown in the following table (excludes reactor units):

Aspen Plus Unit Operation Models Used in the Model

Unit Operation	Aspen Plus Model	Comments / Specifications
Drying and Absorbing Towers	RadFrac	Rigorous absorption including absorption reaction and acid chemistry. Use a “pump around” to model acid-cooling and recirculation
Blower	Compr	Typical pressure rise ~142 in H ₂ O. Comp Block may also be used to model the steam turbine driver if you choose to add one.
Boiler, Superheater, Economizers, Gas-to-Gas Heat Exchangers	MHeatX / HeatX	Using MHeatX block to model heat exchanger usually leads to faster and easier flowsheet convergence. HeatX block supports rigorous design rating or simulation by interfacing with the Aspen Shell & Tube Exchanger program.

Streams - Streams represent the material.

Design-Specs, Calculator Blocks and Convergence - The simulation is augmented with a combination of flowsheeting capabilities such as Convergence, Design Specs and Calculator Blocks.

The following tables outlines the key flowsheeting capabilities used in this model:

Design Specs Used in the Sulfuric Acid Model

Spec Name	Spec (Target)	Manipulated Variables
BURN-SO ₂	Set the SO ₂ Mole Fraction out of SBURN to 0.11	Sulfur (Feed of SBURN) mole flow
DS-1	Set the H ₂ SO ₄ Mass Fraction of product acid IPAT to 0.985	MUWATER (Pure Feed Water to IPAT) mass flow
STEAM	Set the temperature of steam from BLER to 750F	BFWC (Pure Feed Water of EC4A) mass flow

Calculators Used in the Sulfuric Acid Model

Name	Purpose
C-1	Transfers the mass flow unit of stream IP-PRD from lb/hr to tons/day. Shows the temperature profiles of the burner and converters, UA of heat transfer equipment and flow and concentration of production. Uses Excel to perform this calculation. The Excel file is embedded in the file with extension .apmbd.

Note: In the simulation flowsheet, DUPL blocks are used to duplicate streams entered into the heat exchanger. All the duplicated streams are connected to a Hierarchy model in which HeatX blocks are used to simulate heat exchangers. In this way, the flowsheet is not only faster and easier to converge, but supporting rigorous design, rating, or simulation by interfacing with the Aspen Shell & Tube Exchanger program.

Simulation Results:

This simulation will complete with run status “Results Available”. Key simulation results are shown in the following table:

Key Stream Simulation Results:

Flowsheet Variable	Value	Unit
Feed	Air Feed	224000 lb/hr
	Sulfur Feed	26906 lb/hr
	Air/Sulfur	9.36 Mole ratio
	Water for Absorption Column	2236 lb/hr
	Water Steam for Heat Exchange	109164 lb/hr
Product	Sulfuric Acid	83317 lb/hr
	Steam Production	109164 lb/hr
		650 psi
Waste	Exhaust Gas	179826 lb/hr

Process Simulation results:

Process Variable	Value			Unit
Sulfur Burner Temperature	1099			F
Water Content of Feed Air	0.029			Mole Frac
Water Content of Dry Air	5.53			PPM
Converter Temperature	In	Out	Del-T	F
PASS1	750	1114	364	F
PASS2	824	954	130	F
PASS3	810	858	48	F
PASS4	759	802	43	F
SO ₂ in Stack	283			PPM
Sulfuric Acid Concentration	98.5%			Wt
Sulfuric Acid Production	1000			STPD

CONCLUSION

The Sulfuric Acid model provides a useful description of the process. The simulation takes advantage of Aspen Plus's capabilities of modeling electrolyte components. This includes automatic chemistry generation and the capacity of handling electrolyte reactions for all unit models. Aspen Plus provides specialized thermodynamics models and built-in data to represent the non-ideal behavior of liquid phase components in order to get accurate results.

The model may be used as a guide for understanding the process and the economics, and also as a starting point for more sophisticated models for plant designing and process equipment specifying.

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